III B.Tech - II Semester – Regular Examinations – JUNE 2023

DESIGN OF TRANSMISSION ELEMENTS (MECHANICAL ENGINEERING)

Duration: 3 hours

Note: 1. This paper contains questions from 5 units of Syllabus. Each unit carries 14 marks and have an internal choice of Questions.

2. All parts of Question must be answered in one place.

BL – Blooms Level

CO – Course Outcome

Max. Marks: 70

* Use of Approved Design Data book is permitted *

| | | | BL | СО | Max. Marks | |
|---|-----------------------------------------------------------------------|-------------------------------------------------------|----|-----|---------------|--|
| | UNIT-I | | | | | |
| 1 | a) | What are the advantages of hollow shaft over | L2 | CO1 | 2 M | |
| | | solid shaft? | | | | |
| | b) | Find the diameter of a solid steel shaft to transmit | L4 | CO4 | 12 M | |
| | | 20 kW at 200 rpm. The ultimate shear stress for | | | | |
| | | the steel may be taken as 360 MPa and a factor of | | | | |
| | | safety as 8. If a hollow shaft is to be used in place | | | | |
| | | of the solid shaft, find the inside and outside | | | | |
| | | diameters when the ratio of inside to outside | | | | |
| | | diameter is 0.5. | | | | |
| | | OR | | | | |
| 2 | De | sign a muff coupling to connect two steel shafts | L4 | CO4 | 14 M | |
| | | nsmitting 25 kW power at 360 rpm. The shafts and | | | | |
| | | y are made of plain carbon steel 30C8 | | | | |
| | $(S_{yt} = S_{yc} = 400 \text{ N/mm}^2)$. The sleeve is made of grey | | | | | |
| | cast iron FG 200 ($S_{ut} = 200 \text{ N/mm}^2$). The factor of | | | | | |
| | | ety for the shafts and key is 4. For the sleeve, the | | | | |
| | fac | tor of safety is 6 based on ultimate strength. | | | | |
| | UNIT-II | | | | | |
| 3 | Th | e layout of a leather belt drive transmitting 15 kW | L3 | CO2 | 14 M | |
| | of | power is shown in Figure. The center distance | | | | |
| | bet | ween the pulleys is twice the diameter of the | | | | |
| | big | ger pulley. The belt should operate at a velocity of | | | | |

. . .

| | 20 m/s approximately and the stresses in the belt should not exceed 2.25 N/mm ² . The density of leather is 0.95 g/cc and the coefficient of friction is 0.35. The thickness of the belt is 5 mm. Calculate: (i) the diameter of pulleys; (ii) the length and width of the belt; and (iii) the belt tensions. | | | |
|---|----------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------|----|-----|------|
| | 2D | | | |
| 4 | ORa) It is required to select a V-belt drive to connect a 20 kW, 1440 rpm motor to a compressor running | L3 | CO2 | 10 M |
| | at 480 rpm for 15 hours per day. Space is available for a center distance of 1.2 m. Determine (i) the specifications of the belt; | | | |
| | (ii) diameters of motor and compressor pulleys;(iii) the correct center distance; and (iv) the number of belts. | | | |
| | b) Mention the advantages of chain drives compared with belt and gear drives. | L2 | CO1 | 4 M |
| | UNIT-III | | | |
| 5 | a) A single-row deep groove ball bearing is subjected to a radial force of 8 kN and a thrust force of 3 kN. The values of X and Y factors are 0.56 and 1.5 respectively. The shaft rotates at 1200 rpm. The diameter of the shaft is 75 mm and Bearing No. 6315 (C =112000 N) is selected for this application. Estimate (i) Life of the bearing, with 90% reliability; and (ii) Reliability for 20000 h life. | L3 | CO2 | 8 M |
| | b) Discuss the different modes of lubrication in sliding contact bearings. | L2 | CO1 | 6 M |
| | OR | | | |
| 6 | A journal bearing is to be designed for a centrifugal pump for the following data: | L4 | CO4 | 14 M |

| | = | ad on the journal = 12 kN , Diameter of the journal 75 mm, Speed = 1440 rpm , Atmospheric prevature of the oil = 16° C, Operating temperature | | | |
|---|----------------------------------------------------------------------------|----------------------------------------------------------------------------------------------------------------------------------------------------------------------------|----|------------|-------|
| | of the oil = 60° C, Absolute viscosity of oil at 60° C = | | | | |
| | 0.023 kg/m-s. Give a systematic design of the | | | | |
| | bearing. | | | | |
| | | | | | |
| | | UNIT-IV | | | |
| 7 | a) | A centrifugal clutch is to transmit 15 kW at 900 | L3 | CO3 | 10 M |
| | | rpm. The shoes are four in number. The speed at | | | |
| | | which the engagement begins is 3/4th of the | | | |
| | | running speed. The inside radius of the pulley rim | | | |
| | | is 150 mm and the center of gravity of the shoe | | | |
| | | lies at 120 mm from the center of the spider. The | | | |
| | | shoes are lined with ferrodo for which the | | | |
| | | coefficient of friction may be taken as 0.25. | | | |
| | | Determine: (i) Mass of the shoes, and (ii) Size of | | | |
| | | the shoes, if angle subtended by the shoes at the | | | |
| | | center of the spider is 60° and the pressure exerted | | | |
| | 1.) | on the shoes is 0.1 N/mm ² . | 10 | <u>CO1</u> | 4 1 4 |
| | b) | What are requirements of friction material for brake lining? | L2 | CO1 | 4 M |
| | | OR | | | |
| 8 | a) | A multi-disk clutch transmits 50 kW of power at | L3 | CO3 | 7 M |
| | | 1400 rpm. The permissible intensity of pressure | | | |
| | | not to exceed 0.15 N/mm ² , and the coefficient of | | | |
| | | the friction between surfaces is 0.12. the inner | | | |
| | | radius of the discs is 80 mm, and is 0.7 times the | | | |
| | | outer radius. Determine number of disks required | | | |
| | | to transmit the given power. Assume uniform | | | |
| | | wear condition. | | | |
| | b) | A single block brake with a short shoe and torque | L3 | CO3 | 7 M |
| | | capacity of 250 N-m is shown in figure. The | | | |
| | | cylindrical brake drum rotates anti-clockwise at | | | |
| | | 100 rpm and the coefficient of friction is 0.25. | | | |
| | | Find the value of "a" in mm, such that the | | | |
| | | maximum actuating force P is 2000 N. | | | |

| | UNIT-V | | | | | | |
|----|---------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------|----|-----|------|--|--|--|
| 9 | A pair of spur gears consists of a 24 teeth pinion, rotating at 1000 rpm and transmitting power to a 48 teeth gear. The module is 6 mm, while the face width is 60 mm. Both gears are made of steel with an ultimate tensile strength of 450 N/mm ² . They are heat treated to a surface hardness of 250 BHN. Assume that velocity factor accounts for the dynamic load. Calculate (i) beam strength; (ii) wear strength; and (iii) the rated power that the gears can transmit, if service factor and the factor of safety are 1.5 and 2, respectively. | | CO4 | 14 M | | | |
| OR | | | | | | | |
| 10 | a) A pair of spur gears consists of a 20 teeth pinion meshing with a 120 teeth gear. The module is 4 mm. Calculate (i) the center distance; (ii) the pitch circle diameters of the pinion and the gear; (iii) the addendum and dedendum; and (iv) the gear ratio. | L4 | CO4 | 8 M | | | |
| | b) A pair of parallel helical gears consists of a 20 teeth pinion and the velocity ratio is 3:1. The helix angle is 15° and the normal module is 5 mm. Calculate (i) the pitch circle diameters of the pinion and the gear; and (ii) the centre distance. | L4 | CO4 | 6 M | | | |